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TITLE: LOW POWER OSCILLATOR CIRCUIT

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## LOW POWER OSCILLATOR CIRCUIT

### TECHNICAL FIELD

This invention relates to low power oscillator circuits.

### BACKGROUND

A computer typically has a real time clock (RTC) circuit  
5 that resides in the input/output (I/O) controller hub chip,  
sometimes referred to as the "south bridge." In many computers,  
the RTC circuit provides an accurate 32.768 KHz oscillating  
signal that is used to keep the system time whether the computer  
is on or off. The time signal generated by the RTC circuit is  
10 used as a basis to obtain the second, minute, and hour values  
required by the computer.

### DESCRIPTION OF DRAWINGS

Figure 1 is a circuit diagram of a clock oscillator circuit.

Figure 2 is a circuit diagram of a clock oscillator circuit  
15 with a kick-start circuit and an inhibit circuit.

Figure 3 is a block diagram of an electronic device having a  
clock oscillator circuit.

Like reference symbols in the various drawings indicate like  
elements.

### DETAILED DESCRIPTION

20 As will be described in greater detail below, a clock  
circuit includes an inverting amplifier and a resonator  
configured to generate an oscillating signal, and a self-bias  
circuit configured to create a bias voltage to bias the amplifier

in a low-power operating state that can sustain the oscillating signal.

Referring to Fig. 1, a low-power clock oscillator circuit 100 includes a crystal resonator 104, an inverting amplifier 102, a self-bias circuit 106, a sine-to-square wave converter 108, and a low-pass filter 110 (all shown enclosed in dashed lines). Inverting amplifier 102 is designed to provide the necessary gain and phase shift required for oscillation. The self-bias circuit 106 generates a bias voltage at a bias node PBIAS to bias inverting amplifier 102 at a suitable DC operating point. Low-pass filter 110 filters out unwanted noise from the oscillating signal generated at one terminal of resonator 104. Converter 108 serves as an output buffer that generates a square wave having the same frequency as the oscillation frequency of resonator 104. The inverting amplifier 102, self-bias circuit 106, the converter 108, and the filter 110 are all integrated into a single integrated circuit package.

The self-bias circuit 106 has transistors  $M_{n1}$ ,  $M_{p1}$ ,  $M_{n2}$ , and  $M_{p2}$  and a resistor  $R_{bias}$  connected to form a constant biasing circuitry for providing a relatively constant bias current and voltage.  $M_{p1}$ ,  $M_{n1}$ , and  $R_{bias}$  are connected in series and form one leg of the constant biasing circuitry.  $M_{p2}$  and  $M_{n2}$  are also connected in series and form another leg of the constant biasing circuitry. The gate nodes of  $M_{p1}$  and  $M_{p2}$  are connected through node PBIAS, and the gate nodes of  $M_{n1}$  and  $M_{n2}$  are connected through node VBIAS. The drain and gate nodes of  $M_{n2}$  are

connected, and the drain and gate nodes of  $M_{p1}$  are connected. This arrangement produces a relatively constant current  $I_1$  flowing through  $M_{p1}$  and  $M_{n1}$ , and a relatively constant current  $I_2$  flowing through  $M_{p2}$  and  $M_{n2}$ .

5 Inverting amplifier 102 includes transistors  $M_{n3}$  and  $M_{p3}$ . The gate nodes of  $M_{p1}$ ,  $M_{p2}$ , and  $M_{p3}$  are connected together through node PBIAS. The sizes (i.e., the width/length ratios of the channels) of  $M_{n1}$ ,  $M_{p1}$ ,  $M_{n2}$ ,  $M_{p2}$ ,  $M_{n3}$ , and  $M_{p3}$  and the resistance value of  $R_{bias}$  are selected so that  $M_{n1}$ ,  $M_{p1}$ ,  $M_{n2}$ ,  $M_{p2}$ ,  $M_{n3}$ , and  $M_{p3}$  all operate at a  
10 sub-threshold level while still sustaining oscillation. In the following description, a circuit is said to be in a "low power" state when the transistors in the circuit are operating in sub-threshold levels.

The current  $I_1$  is determined by the relative size difference  
15 between  $M_{n1}$  and  $M_{n2}$ , the relative size difference between  $M_{p1}$  and  $M_{p2}$ , and resistor  $R_{bias}$ . In the described example, the size of  $M_{p1}$  is selected to be equal to the size of  $M_{p2}$  so that the magnitude of currents  $I_1$  and  $I_2$  are substantially the same. This allows the bias circuit to function properly while using less current than  
20 other configurations. The size ratio between  $M_{p3}$  and  $M_{n3}$  is similar to the size ratio between  $M_{p2}$  and  $M_{n2}$ , except that  $M_{p3}$  and  $M_{n3}$  are configured to be three times greater than the size of  $M_{p2}$  and  $M_{n2}$ , respectively. The DC voltage at the gate node of  $M_{n2}$  is thus similar to the DC voltage at the gate node of  $M_{n3}$ , and the

current  $I_3$  flowing through  $M_{p3}$  and  $M_{n3}$  is about three times as much as  $I_1$ . A higher operation current is used for inverting amplifier 102 in order to provide sufficient gain so that the oscillator loop gain is always greater than one under various operating conditions. A lower operation current is used for self-bias circuit 106 in order to reduce power consumption.

Due to manufacturing tolerances, there may be mismatches between the various transistor devices. To ensure reliable performance, self-bias circuit 106 and inverting amplifier 102 are configured to have the DC gate voltage of  $M_{n3}$  slightly higher than the voltage at node VBIAS. This is achieved by making transistor  $M_{p3}$  slightly greater than three times that of  $M_{p2}$  to account for layout geometry mismatches that may affect the loop gain.

Crystal resonator 104 has two terminals,  $X_1$  and  $X_2$ , that are connected to input and output terminals, respectively, of inverting amplifier 102. The input terminal of inverting amplifier 102 is the gate node of  $M_{n3}$ , and the output terminal of inverting amplifier 102 is the drain node of  $M_{n3}$ . A feedback resistor  $R_f$  is connected in parallel to resonator 104. The value of  $R_f$  is selected so that inverting amplifier 102 achieves optimal gain for oscillation. Capacitors  $C_1$  and  $C_2$  are connected to terminals  $X_1$  and  $X_2$ , respectively, to add phase shift that is necessary for oscillation. The values of these load capacitors are chosen based on the electrical characteristics of the crystal resonator 104.

In the described example, resonator 104 is selected to resonate at approximately 32.77 KHz, resistor  $R_i$  is selected to have a value of about 10 Meg-Ohms, and capacitors  $C_1$  and  $C_2$  are selected to have capacitances of about 18 pF.

5        An advantage of a low-power clock oscillator having this arrangement and operated in this way is that when inverting amplifier 102 and self-bias circuit 106 are packaged in an integrated circuit (IC) package, the connection between inverting amplifier 102 and self-bias circuit 106 are contained entirely  
10        within the IC package. Because self-bias circuit 106 is not connected to any external components, self-bias circuit 106 is less likely to be influenced or affected by the environment outside of the IC package. The clock oscillator circuit 100 is thus more accurate and less likely to fail. Moreover, without the  
15        need to have additional connections to outside components, these pins can be used for other functions.

Another advantage of the invention is that the capacitance associated with node VBIAS is very small (on the order of femto Farads). Compared to previous designs that require connection of  
20        external components to provide feedback to the bias circuit, the invention allows node VBIAS to be charged faster and the DC bias voltage to be established faster, thereby allowing inverting amplifier 102 and resonator 104 to start oscillation faster. By not using any external component to generate feedback for the  
25        bias circuit, leakage current and external influences (e.g., influences from the environment or a human operator) is

significantly reduced so that the clock signal is more accurate and less likely to fail at start-up.

A further advantage of the invention is that self-bias circuit 106 and inverting amplifier 102 can both operate at a low power state that consumes a very low amount of power. Transistors  $M_{n1}$ ,  $M_{p1}$ ,  $M_{n2}$ ,  $M_{p2}$ ,  $M_{n3}$ , and  $M_{p3}$  are configured to operate at sub-threshold levels while sustaining oscillation to provide a system clock signal. This is particularly important because the RTC circuit must operate on battery power when the system power is turned off.

The circuit configuration described above can function properly across a large range of process, voltage, and temperature conditions. For example, if  $V_{cc}$  increases, the clock oscillator circuit 100 will still provide accurate clock signal. This is because of the size ratios of the transistor pairs (i.e.,  $M_{p1}:M_{n1}$ ,  $M_{p2}:M_{n2}$ ;  $M_{p3}:M_{n3}$ ) are the same, thus any influence by process, voltage, or temperature will have the same effect on the transistor pairs. Characteristics of the circuit, e.g., trip point and DC voltage levels, will change by the same amount for the inverting amplifier 102, the self-bias circuit 106, and the converter 108.

Low-pass filter 110 includes a resistor  $R_{filter}$  and a capacitor  $C_{filter}$ . Low-pass filter 110 filters out unwanted noise from the oscillating signal generated at terminal  $X_1$  of resonator 104, so that a filtered sinusoidal signal having the desired oscillating frequency is sent to converter 108. Converter 108 converts the filtered sinusoidal signal into a square wave. Converter 108 also

serves as a buffer to prevent output load variations from affecting the stability of the frequency of the clock oscillator circuit 100.

Converter 108 includes transistors  $M_{n4}$  and  $M_{p4}$  that are configured to operate in a way similar to an inverting amplifier. The gate node of  $M_{n4}$  is connected to terminal  $X_1$ , and the gate node of  $M_{p4}$  is connected to node PBIAS. The size ratio between  $M_{p4}$  and  $M_{n4}$  is designed to be the same as the size ratio between  $M_{p3}$  and  $M_{n3}$  so that the trip point for the  $M_{p4}$ - $M_{n4}$  transistor pair is the same as that for the  $M_{p3}$ - $M_{n3}$  inverting amplifier. The trip point refers to the voltage level where the input voltage of the input amplifier equals the output voltage. The square wave generated by converter 108 has rail-to-rail voltage swings and is used to drive other logic circuits.

Self-bias circuit 106 has two stable operating states, a normal operating state and a zero current operating state. In one example,  $M_{n1}$  and  $M_{n2}$  are configured so that the leakage current of  $M_{n1}$  is greater than  $M_{n2}$ . Then the bias circuit will usually remain in the normal operating state. In an alternative example, a kicker circuit (or called an excitation circuit) is used to provide an excitation to enable self-bias circuit 106 to operate at its normal operating state.

Referring to Figure 2, a low power clock oscillator circuit 200 includes a resonator 104, an inverting amplifier 102, a self-bias circuit 106, and a self-timed kicker circuit 202. The kicker circuit 202 "kick-starts" self-bias circuit 106 by providing an



excitation to self-bias circuit 106 when power is initially applied, and to inhibit the excitation when inverting amplifier 102 is able to sustain oscillation. The circuit 202 is similar to the circuit described in U.S. Patent No. 6,191,662 B1, "Self-  
5 Start Circuits for Low-Power Clock Oscillators." The inverting amplifier 102, the self-bias circuit 106, and the kicker circuit 202 are all integrated into a single integrated circuit package.

When a logic high TRIGGER signal is applied to the gate node of a transistor  $M_7$ , transistor  $M_7$  is turned on and causes  
10 transistors  $M_8$ ,  $M_9$ , and  $M_{10}$  to turn on. This enables a small current to be drawn to ground from node PBIAS through transistors  $M_8$  to  $M_{10}$ . This current is an excitation signal that excites currents in transistors  $M_{p1}$ ,  $M_{p2}$ , and  $M_{p3}$ , thereby allowing currents  $I_1$  and  $I_2$  to start flowing through self-bias circuit  
15 106, and current  $I_3$  to start flowing through inverting amplifier 102. Eventually, current  $I_3$  grows large enough to be able to sustain oscillation of resonator 104.

The clock oscillator circuit 200 can self-start and sustain oscillation of resonator 104 when there is sufficient current in  
20 transistor  $M_{p3}$  to overcome any other source of leakage current towards the ground node. This condition will occur when transistor  $M_{n2}$  is conducting current above a few nano-amperes (depending on the manufacturing process). Because the current gain between transistors  $M_{p3}$  and  $M_{p2}$  is designed to be about 3,  
25 the current in transistor  $M_{p3}$  is about 3 times the current flowing through  $M_{p2}$  when resonator 104 starts to oscillate.

In order to inhibit the excitation when inverting amplifier 102 can sustain oscillation of crystal resonator 104, a "current mirror" that includes  $M_{11}$  and  $M_{12}$  is used to sense the current flowing in transistor  $M_{n2}$ . Transistor  $M_{12}$  is appropriately sized to pull a SENSE node to logic low when current conducting in transistor  $M_{n2}$  is sufficient to overcome the leakage current. Transistor  $M_{11}$  enables the mirror circuit when the TRIGGER signal is asserted to logic high. When the voltage at the SENSE node is pulled low, the current flowing through transistors  $M_8$  to  $M_{10}$  is shut off.

The mirror circuit monitors the rise of voltage on the PBIAS node after power is applied and the TRIGGER signal is asserted. The current flowing through  $M_8$  to  $M_{10}$  is shut off as soon as transistor  $M_{n2}$  is conducting sufficient current to sustain oscillation. After the voltage on the SENSE node transitions to logic low, the presence or removal of the TRIGGER signal has no further effect on the self-bias circuit 106 and inverting amplifier 102. Further, if resonator 104 is already oscillating and inverting amplifier 102 is already functioning when the TRIGGER signal is applied, the voltage on the SENSE node will already be low and remain low. Thus, the kicker circuit 202 will not affect self-bias circuit 106 regardless of the logic state of the TRIGGER signal.

Referring to Fig. 3, an electronic device 300 includes a low-power clock oscillator circuit 200 that provides a stable clock signal. Clock oscillator circuit 200 has a self-bias

circuit to bias the clock oscillator circuit 200 into a low-power state. The circuit 200 includes circuitry to provide kick-start function during power-up, and circuitry to inhibit kick-start when oscillation is sustained or if the oscillator is already running. The electronic device 300 further includes a processor 302, a bus system 304, a display device 306, a memory device 308, and input/output (I/O) devices 310. The low-power clock oscillator circuit 200 keeps time during periods when the rest of the system is powered down or powered off.

A number of embodiments of the invention have been described. Nevertheless, it will be understood that various modifications may be made without departing from the spirit and scope of the invention. For example, the self-bias circuit may be any type of constant biasing circuitry that can provide an appropriate DC bias voltage at the bias node, as long as the circuitry allows the characteristics (e.g., trip point, gain, current) to scale similarly for the inverting amplifier, the self-bias circuit, and converter across a range of process, voltage, and temperature conditions. The channel types for the transistors shown in Figs 1 and 2 may be different, and the N-type and P-type transistors may be interchanged without affecting the functionality of the circuit. Electronic device 300 may be a computer, a handheld device, or any other device that needs to keep a system clock signal while the main power is turned off.

The sizes of transistors  $M_{p1}$ ,  $M_{p2}$ ,  $M_{n1}$ ,  $M_{n2}$  can be selected so that currents  $I_1$  and  $I_2$  are different. For example, if the size of  $M_{p1}$  and  $M_{n2}$  are selected as  $W/L$ , the size of  $M_{n1}$  selected as

$M \cdot W/L$ , and the size of  $M_{p2}$  selected as  $K \cdot W/L$ , then

$I_1 = (V_T/R) \cdot \ln(M \cdot K)$ , and  $I_2 = K \cdot I_1$ , where  $V_T$  is the thermal voltage

(approximately 26 mV at room temperature), and  $R$  is the resistance value of resistor  $R_{bias}$ . Accordingly, other embodiments

5 are within the scope of the following claims.

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